

# Calibrating Optical Sensors for Semiconductor Process Control

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**Verity**  
INSTRUMENTS, INC.

SPECTROGRAPHY  
ADVANCED PROCESS CONTROL

PLASMA DIAGNOSTICS



# Outline

- Integrated optical sensors for semiconductor process control
- Sources of drift and variation
- Broadband radiometric calibration method



# Integrated Metrology

- Integrated measurement philosophy
  - Data now rather than later (W2W instead of L2L)
  - Integrated metrology localizes problems in real-time for greatest financial impact<sup>1</sup>
- What are unique challenges for integrated metrology?
- Focus on optical sensors
  - Primarily optical emission spectroscopy (OES) and reflectometry

<sup>1</sup> – Charles Weber, “Strategic Options for Users and Suppliers of APC Technology”, Integrated Metrology Association Meeting, San Francisco, CA, 1999



# Integrated Optical Sensors

- OES for endpoint detection
  - Historically interference filter or monochromator based
  - Now spectrographs and multivariate algorithms
- OES for emerging applications
  - Chamber matching<sup>2</sup> and fault detection<sup>3</sup> place new demands on OES
- Reflectometry
  - Wafer state endpoint monitor for deposition and CMP<sup>4</sup>
  - “Similar” hardware for scatterometry

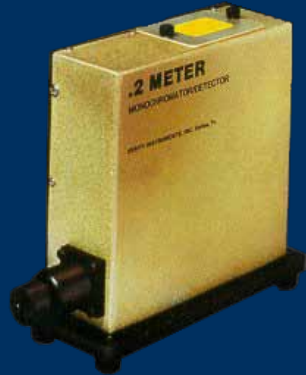
<sup>2</sup> – ISMI Equipment Chamber Matching (ECM) Project

<sup>3</sup> – H. H. Yue et al., *IEEE Trans. Semi. Manu.*, **13**, No. 3, Aug. 2000, Pg. 374-385

<sup>4</sup> – Jeff David et al., *8<sup>th</sup> European AEC/APC Conference, Dresden, Germany, April 2007*



# Verity Instruments Product Overview



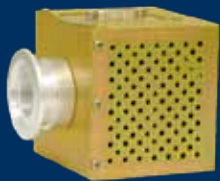
Monochromator



System Controller



Spectrographs  
(UV-VIS & NIR)



Interference  
Filter Detector



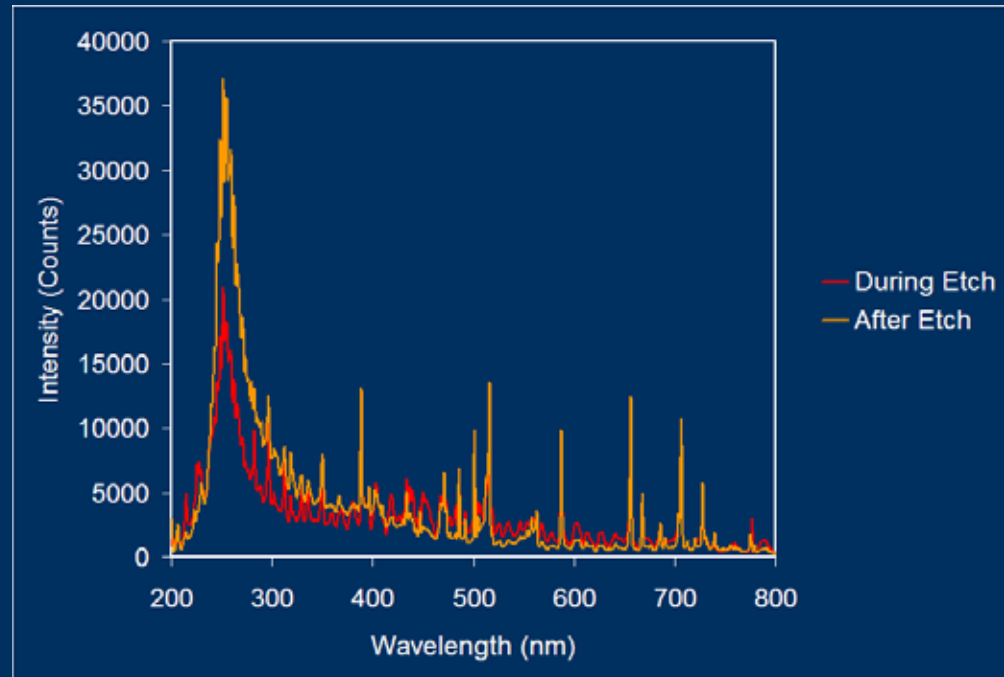
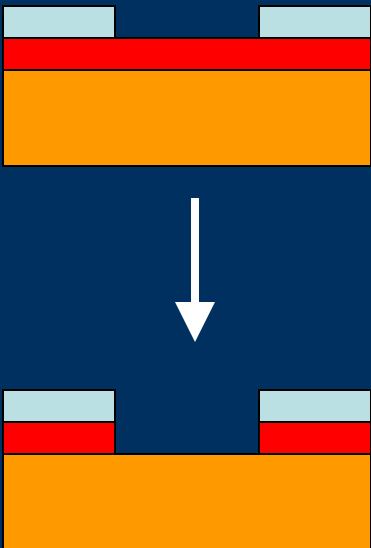
System Controller



Spectral  
Reflectometer



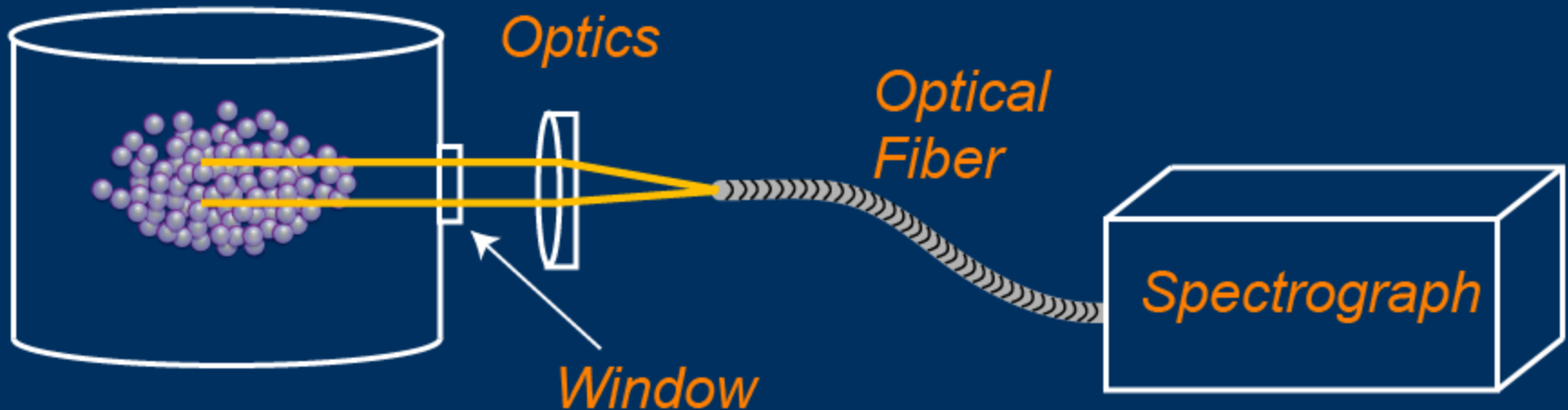
# OES Endpoint



- During etch, plasma emission spectrum changes as etch layer is cleared → endpoint
- Magnitude of change depends on etch chemistry, open area, layer material, etc.



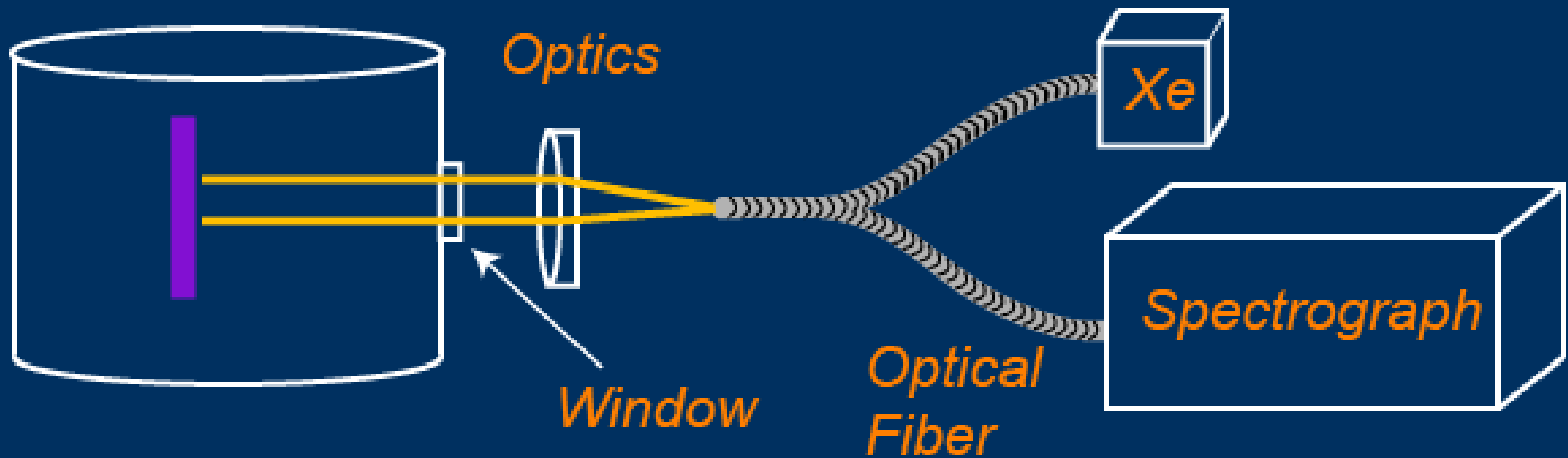
# Integrated Optical Systems: OES



- Four primary sub-systems in OES path (window, optics, fiber, spectrograph)



# Integrated Optical Systems: Reflectometry



- Same sub-systems as OES (window, optics, fiber, spectrograph) plus Xe flashlamp



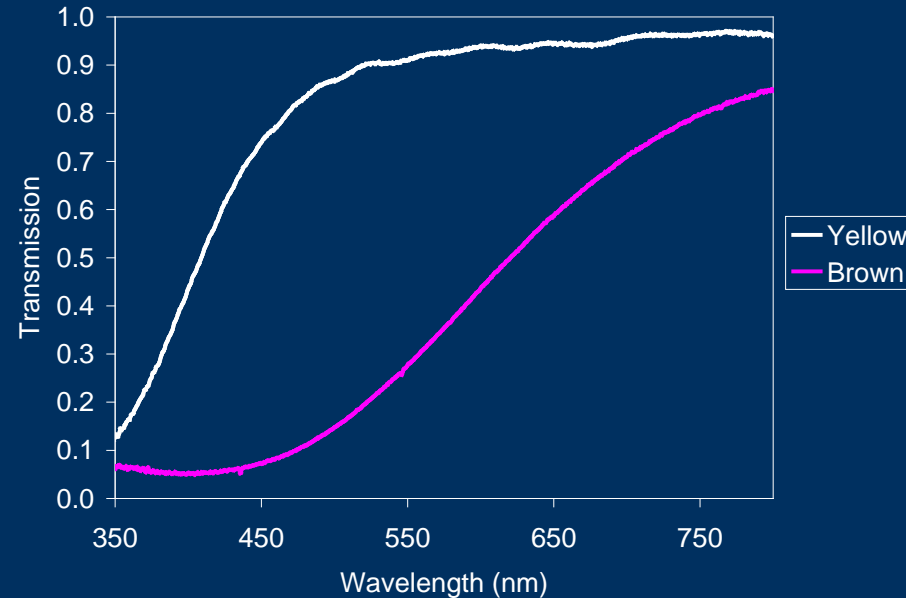
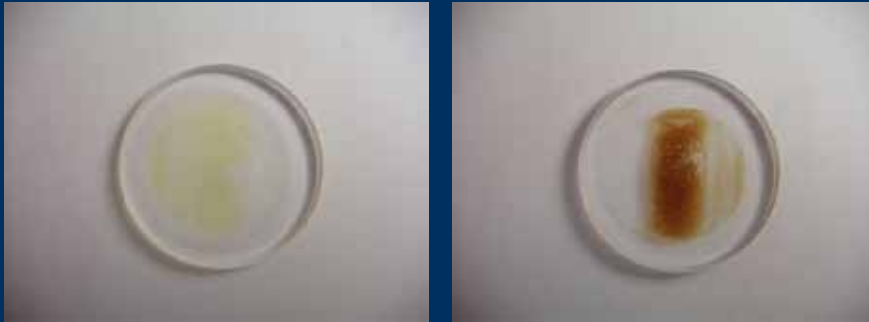


# What are the Challenges?

- *In-situ* environment is harder to control
  - That is, process chambers are messy (e.g. reactive chemistries, wet, hot, vibration, etc.)
    - à Sources of drift
- Use of calibration standards *in-situ* can be very difficult
  - à Unit-to-unit repeatability is important
- In light of all this, high gage capability is still required



# Window Transmission



- Re-deposition of particulate causes clouding à drift
- Depends on chamber geometry and process
- $\frac{D\text{Transmission}}{D\text{Time}}$  can approach 20%/day



# Chamber Coupling Optics

- Most common are direct (no lenses) and simple focusing lenses
- Reflectometry often used with collimating lenses
- Mostly susceptible to unit-to-unit variations
  - Geometric alignments
  - Lens tolerances
  - Broadband AR coatings (if applicable)
- Specific to each installation



# Optical Fibers

- Most convenient means to transfer signal from chamber to spectrograph
- Available with good transmission down to  $\lambda \sim 193\text{nm}$
- Subject to drift primarily from solarization in the UV
- And subject to unit-to-unit variation primarily from coupling geometry



# Fiber-to-Spectrograph Coupling

$$\text{Coupling} \approx I_0 \cdot \delta \cdot D_F \left[ 1 - \frac{2(X_F - X_S)^2}{D_F^2} \right] \cdot T(\lambda)$$

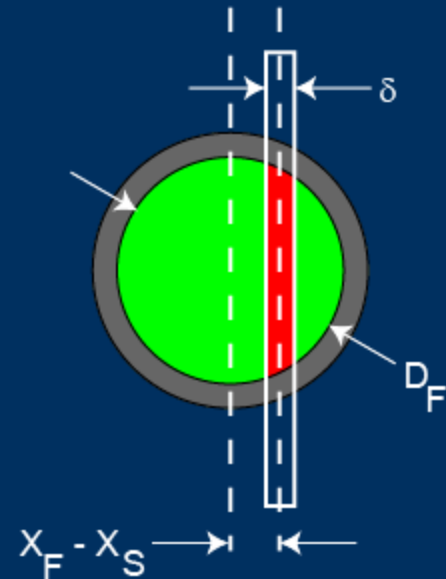
$I_0$  = Irradiance leaving fiber in W/cm<sup>2</sup>

$\delta$  = Slit width

$D_F$  = Fiber core diameter

$X_F - X_S$  = Transverse offset from fiber to slit

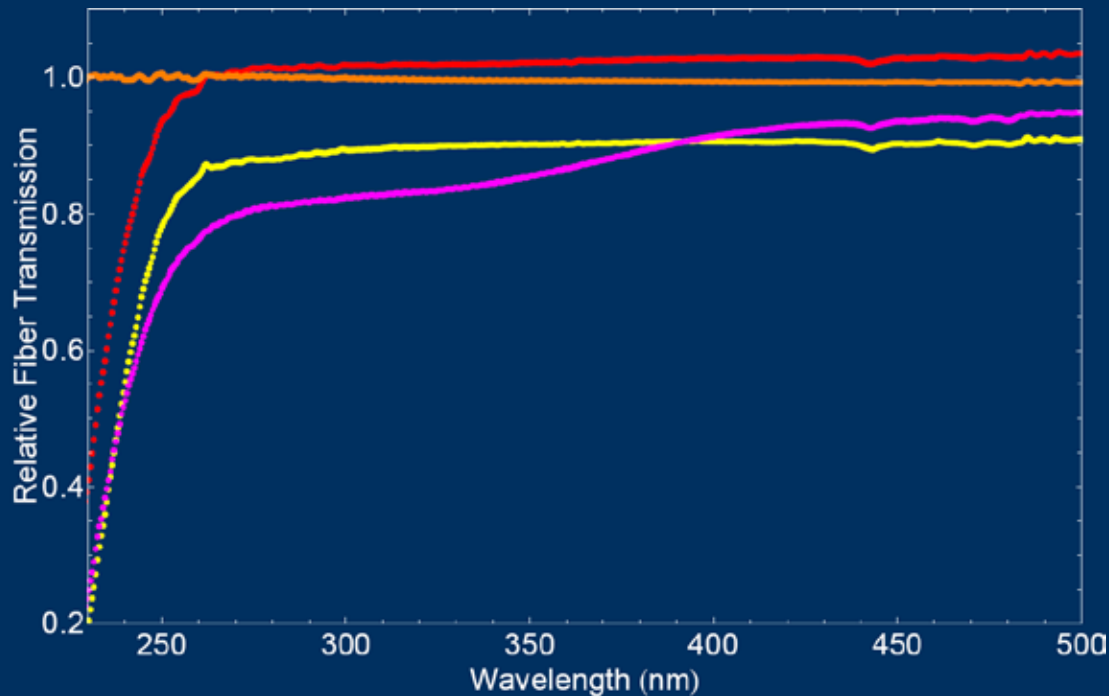
$T(\lambda)$  = Transmission of fiber



- Red overlap region is signal collected by spectrograph (“Coupling”)
- To lowest order coupling depends on transverse errors from slit to fiber core



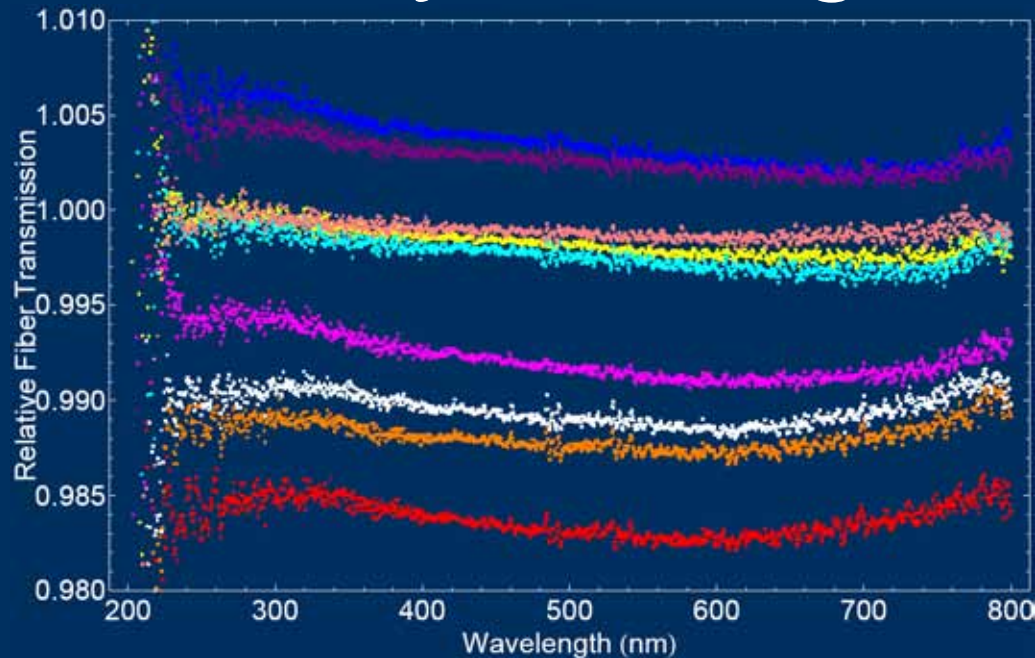
# Variation Between Fibers



- Four different fibers measured relative to a (new) fifth
- $D_F = 200\text{mm}$ ,  $X_F - X_S = \pm 0.002''$  à  $\approx 13\%$  variation unit-to-unit
- Solarization gives rise to up to 80% drift variation in deep UV



# Repeatability of Single Fiber



- Take one fiber and measure multiple repeat installations
- Mechanical connection variations and bend losses create unit-to-unit variation
- “Worst” case is ~5% (primarily due to bend losses), and careful control limits this to under 2% (as shown)



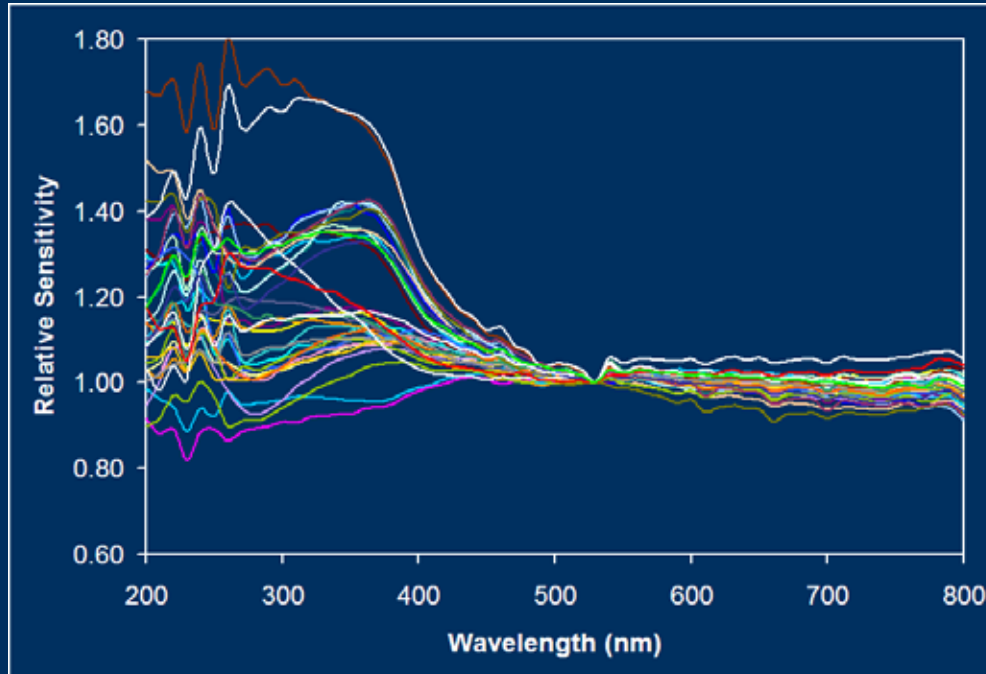
# Xe Flashlamp

- Long-life (typically  $>1E9$  shots), very broadband (190-2100nm) source
- Unit-to-unit variation
  - Overall intensity (easily accommodated with drive voltage)
- Drift
  - Decrease in intensity (again, adjust voltage)
- Generally very robust light sources for reflectometry applications





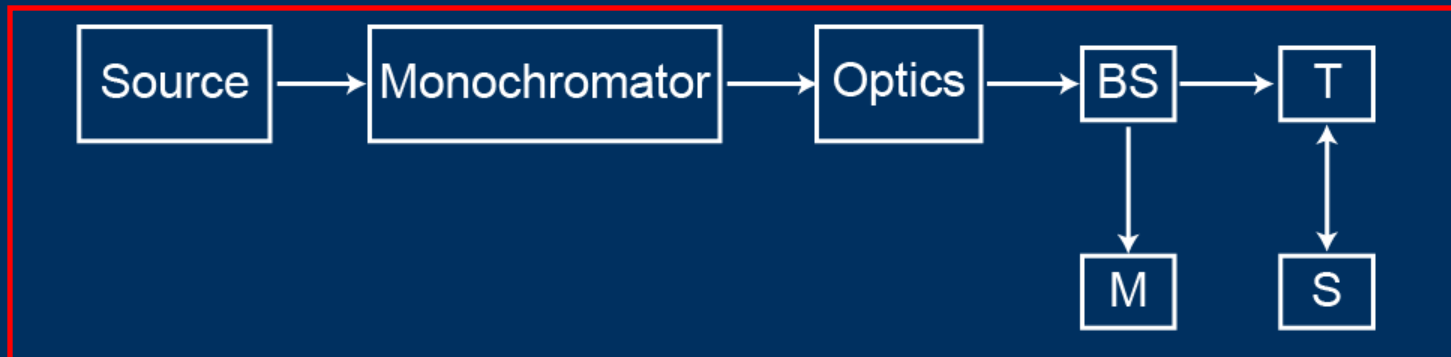
# Spectrographs



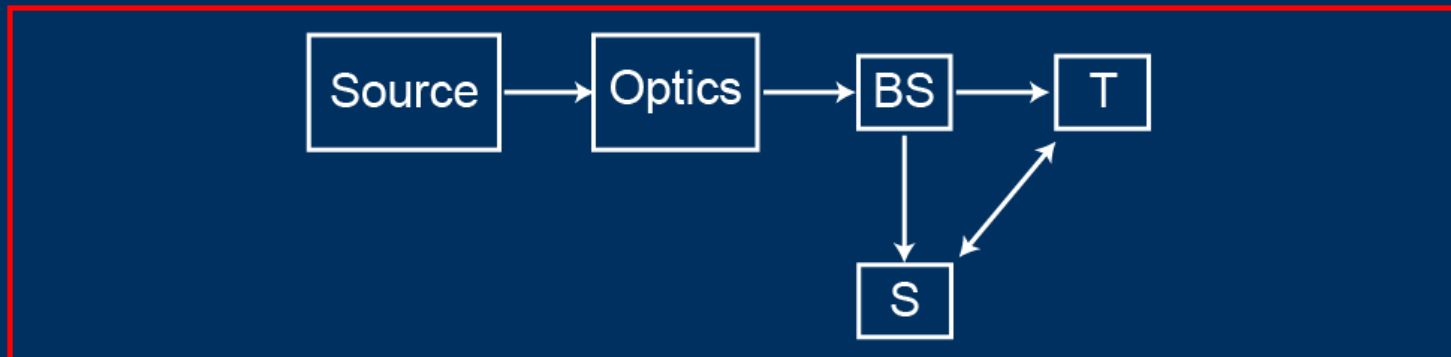
- Unit-to-unit variations
  - Calibration of I
  - Sensitivity calibration
- Drift sources
  - Temperature
  - Vibrations
  - Component creep
- Several design elements involved in minimizing these, but let's discuss sensitivity calibration



# Adapted Substitution Method with Monitor



Original<sup>5</sup>



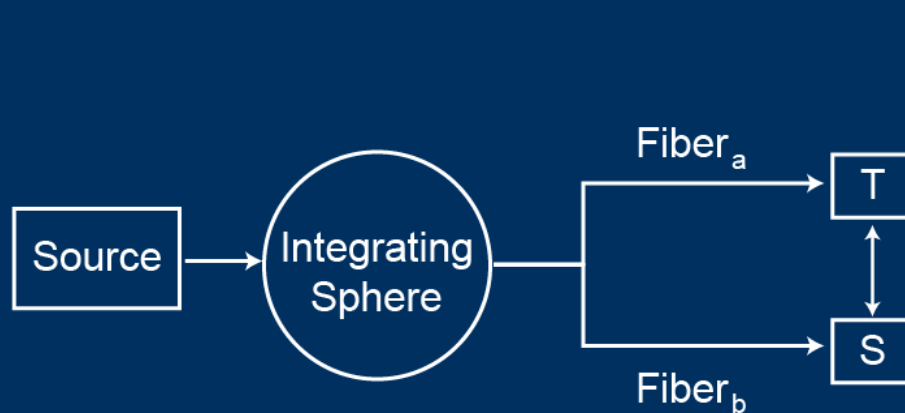
Adapted

- S & T are spectrographs, so can eliminate monochromator
- Standard can serve as monitor

<sup>5</sup> – Larason, Bruce, and Parr, "Spectroradiometric Detector Measurements", NIST Special Publication 250-41, 1998



# Implementation & Measurement Equation



$$V_T^{(1)} = S_T \cdot \tau_a \cdot \Phi^{(1)}$$

$$V_S^{(1)} = S_S \cdot \tau_b \cdot \Phi^{(1)}$$

$$V_T^{(2)} = S_T \cdot \tau_b \cdot \Phi^{(2)}$$

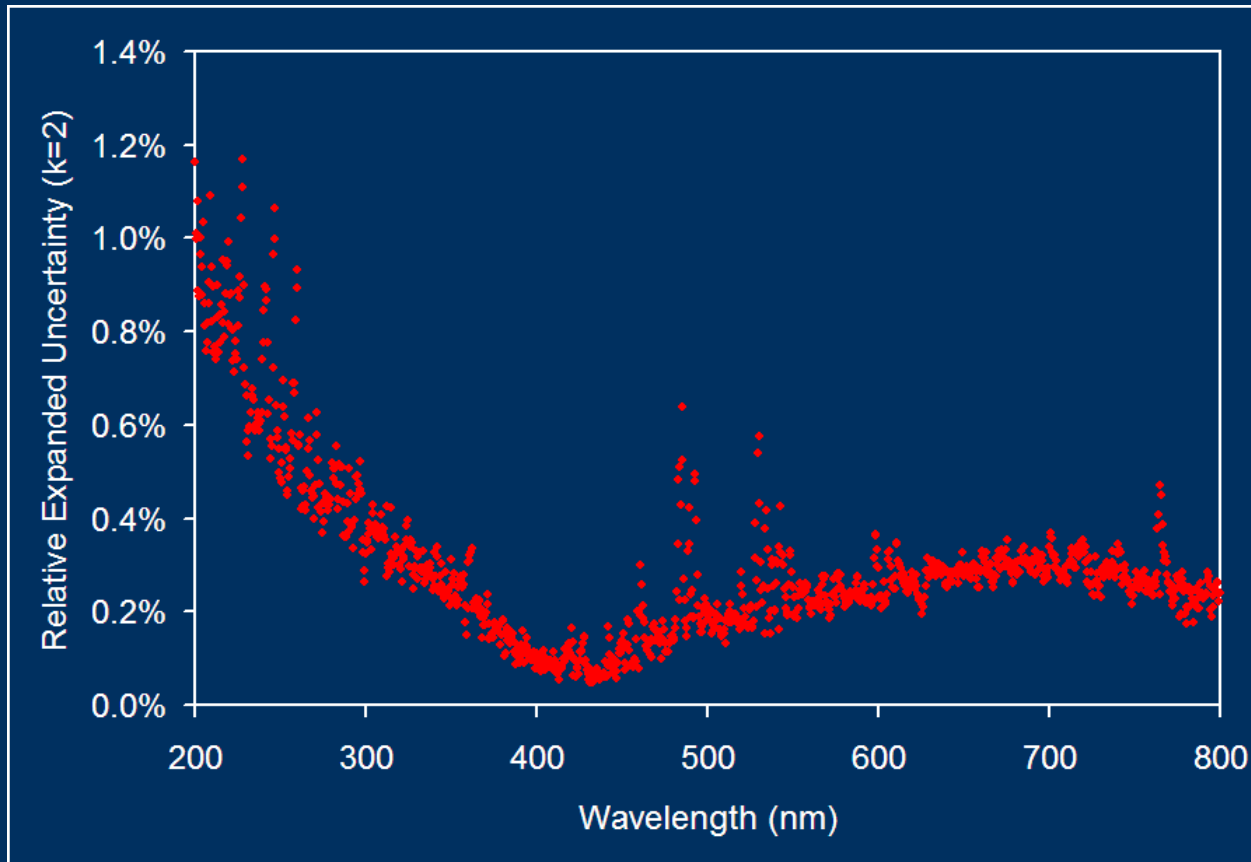
$$V_S^{(2)} = S_S \cdot \tau_a \cdot \Phi^{(2)}$$

$$S_T = \sqrt{\frac{V_T^{(1)} \cdot V_T^{(2)}}{V_S^{(1)} \cdot V_S^{(2)}}} \times S_S$$

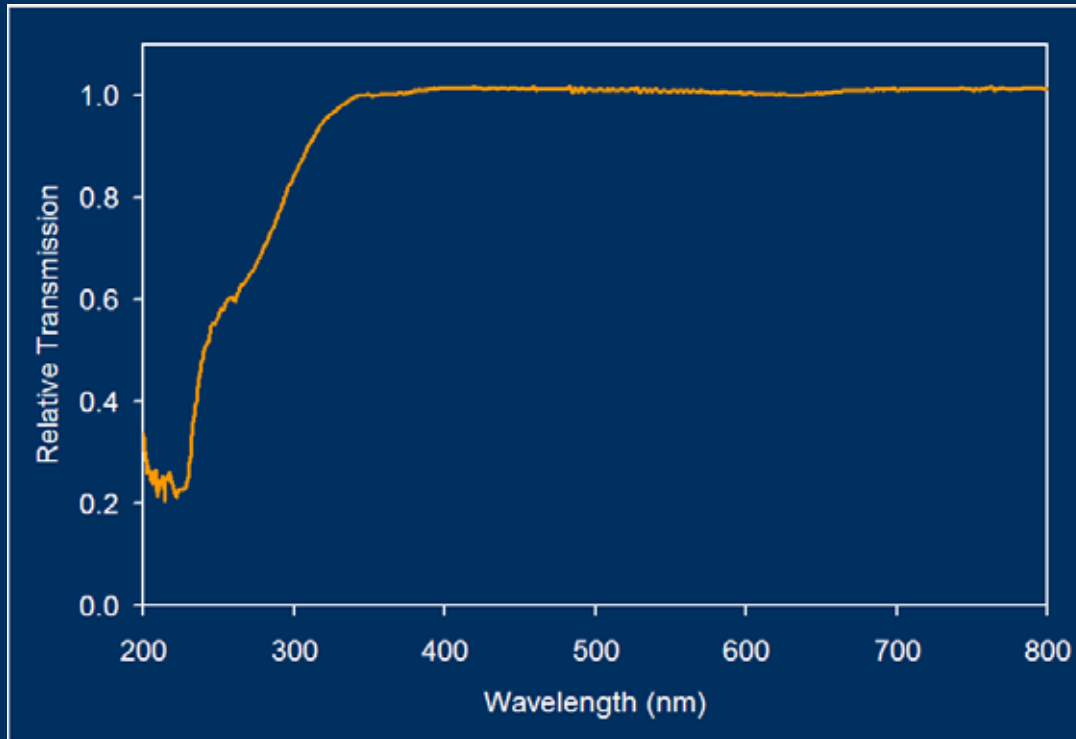
- Modification of standard measurement equation adapted for this approach
- Differential fiber to slit coupling contributes an overall offset (wavelength independent)
- Can use Xe flashlamp as source



# Spectral Responsivity Measurement Uncertainty



# Characterizing Fiber Transmission



$$\frac{\tau_a}{\tau_b} = \sqrt{\frac{V_T^{(1)} \cdot V_S^{(2)}}{V_S^{(1)} \cdot V_T^{(2)}}}$$

- Combining four measurements differently can give ratio of transmissions of two optical sub-systems
- Shown here as a method to characterize fiber solarization



# Conclusion

- In semiconductor process control, integrated optical sensors play an important role in yield management and factory efficiency
- We have reviewed some of the sources of drift and variation in these sensors
- A broadband radiometric calibration process was described that allows low uncertainty and a convenient measurement method

