Study of Non-Uniformity Corrections in Luminous Flux Measurements of Automotive Headlamps using an Integrating Sphere through Simulations

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Development and Manufacturing of automotive lights since 1976 in Brazil

2 Sites / ~ 500 employees / ~ 2000 products / IATF / ISO 9001 / **ISO 17025 (Photometry)**

Website: www.pradolux.com

Example of products:



Tail lights



Head lights



Markers



Equipment

Integrating Sphere, diameter = 1.5 m (*Everfine*)

Spectroradiometer HAAS-2000, 350-1000nm (*Everfine*)

Gonio-photometer type A (automotive) with class A (3%) photometer (*Everfine*)





1. The problem of spatial non-uniformity

Example of light - Sample #1 1.100 1.075 1.050 30° ^{20° 10° 0°} -10° -20° 1.025 -30° 40° 50° -50° 1.000 60° -60° 70° -70° 0.975 -80° 0.950 .90° 0.0 0.2 0.4 0.6 0.8 1.0 -150-100

80°

90°



Relative Luminous Flux – Sample #1



2. Simulations of the SRDF for our device[1]

- Build the model of the sphere (baffle, table, holders, detector, aux. lamp, etc.)
- Set all surfaces as Lambertian with a constant reflectivity ho
- Divide the sphere into 2,592 elements (5° step on θ and ϕ)
- Each element is illuminated by a lamp and the rays are traced with the reflections to the detector (with 180° and cosine angular responsivity)
- The detector response is recorded in a function $K = K(\theta, \phi)$
- The SRDF is normalized as

$$K^*(\theta,\phi) = \frac{4\pi K(\theta,\phi)}{\int_{\phi=0}^{2\pi} \int_{\theta=0}^{\pi} K(\theta,\phi) \sin\theta d\theta d\phi}$$







Modeling the sphere for ray-tracing







Ray-tracing engine – Raysect[2]



3. Analysis of the best reflectivity model







Simulated SRDF for different reflectivity values at $\theta = 90^{\circ}$







Flux correction due to the non-uniformity [1]

Sphere response factor

$$f_{s} = \frac{\int_{\phi=0}^{2\pi} \int_{\theta=0}^{\pi} K^{*}(\theta,\phi) I_{DUT}(\theta,\phi) sin\theta d\theta d\phi}{\int_{\phi=0}^{2\pi} \int_{\theta=0}^{\pi} I_{DUT}(\theta,\phi) sin\theta d\theta d\phi}$$

where, $I_{DUT}(\theta, \phi)$ is the Luminous Intensity of the Device Under Test (neglecting correction from the reference lamp)

Correction factor
$$k_s = \frac{1}{f_s}$$



5 Headlights with different LIDs





Measurement region



Optical axis parallel to the horizontal plane



Example of corrections for different reflectivity values







Accuracy of the corrected fluxes for different reflectivity values





Best model for SRDF, $\rho = 92,5\%$





4. Corrections





The correction in the flux model [3]

$$\Phi = \Phi_R \cdot \frac{y}{y_R} \cdot \frac{y_{AR}}{y_A} \cdot \left(\frac{U \cdot c_U}{U_0}\right)^{m_U} \cdot \left(\frac{J_R \cdot c_R}{J_0}\right)^{m_{J_R}} \cdot \frac{corS_R}{corS}$$

where:

Φ_R is the flux of the reference lamp

 $\frac{y}{y_R}$ is the factor of the signal of the test sample and the reference lamp

 $\frac{y_{AR}}{y_A}$ is the self-absorption correction

 $\left(\frac{U.c_U}{U_0}\right)^{m_U}$ is the correction of the measurement voltage of the test sample

 $\left(\frac{J_R.c_R}{J_0}\right)^{m_{J_R}}$ is the correction of the measurement current of the reference lamp

The correction in the flux model [3] (cont.)

$$\Phi = \Phi_R \cdot \frac{y}{y_R} \cdot \frac{y_{AR}}{y_A} \cdot \left(\frac{U \cdot c_U}{U_0}\right)^{m_U} \cdot \left(\frac{J_R \cdot c_R}{J_0}\right)^{m_J} \cdot \frac{corS_R}{corS}$$
where:

$$corS_R = (1 + \alpha_R \Delta T_{\alpha R} - \Delta s f_R - S_R - \gamma_R \Delta t_R)$$

$$corS = (1 + \alpha \Delta T_\alpha - \Delta s f - S - \gamma \Delta t)$$
where:

$$\alpha$$
 is the relative temperature coefficient,

$$3\%$$
 correction

wh

α

 ΔT_{α} is the difference in ambient temperature during the measurement,

 Δsf is the non-uniformity factor of the sphere: (k_s-1),

S is the factor of the influence of stray light,

 γ is the luminous flux decrease coefficient due to source aging,

 Δt is the total source usage time.

(Calibrated reference denoted with the subscript *R*)

		Relative	Relative
Symbol	Туре	u _{rel} (y)	u _{rel} (y)
		Headlamp	Isotropic
∆Ta	В	0,02%	0,02%
α	В	0,00%	0,00%
Δsf	В	-1,56%	-0,05%
S(θ)	В	-0,21%	-0,21%
γ	В	-0,69%	-0,69%
corS		1,71%	0,70%
$\Delta T_{\alpha R}$	A	0,02%	0,02%
α R	В	0,00%	0,00%
∆sfR	В	-0,05%	-0,05%
S _R (<i>θ</i>)	В	-0,20%	-0,20%
уr	В	-0,01%	-0,01%
corS _R		0,21%	0,21%
Φ_R	В	2,10%	2,10%
у	А	0,82%	0,82%
y _R	А	-0,02%	-0,02%
УА	А	-0,74%	-0,74%
YAR	А	0,02%	0,02%
U	А	0,09%	0,09%
CU	В	-0,11%	-0,11%
mυ	В	0,00%	0,00%
U _R	А	0,71%	0,71%
CR	В	0,34%	0,34%
m _{JR}	В	-0,07%	-0,07%
Φ		3,04%	2,61%
	k=2	6,08%	5,22%

$$\Phi = \Phi_R \cdot \frac{y}{y_R} \cdot \frac{y_{AR}}{y_A} \cdot \left(\frac{U \cdot c_U}{U_0}\right)^{m_U} \cdot \left(\frac{J_R \cdot c_R}{J_0}\right)^{m_{J_R}} \cdot \frac{corS_R}{corS}$$

$$Y = \Phi \left(\Phi_{R}, y, y_{R}, y_{AR}, y_{A}, U, c_{U}, m_{U}, J_{R}, c_{R}, m_{J_{R}}, \alpha_{R}, \Delta T_{\alpha R}, \Delta s f_{R}, S_{R}, \gamma_{R}, \Delta t_{R}, \alpha, \Delta T_{\alpha}, \Delta s f, S, \gamma, \Delta t \right)$$

GUM (Guide to the expression of uncertainty in measurement)[5]

$$u_{c}(y) = \sqrt{\sum_{i=1}^{N} \left(\frac{\partial f}{\partial x_{i}}\right)^{2} u^{2}(x_{i})} \qquad N = 23$$
 Sample #3

5. Conclusions and outlook

- Errors in luminous flux measurements of headlights due to spatial non-uniformity in the integrating sphere are not small and must be corrected.
- ✓ The SRDF of our sphere was simulated with various details using the method described by Ohno et al [1].
- ✓ It was demonstrated, with measurements from 5 samples, that the model with 92.5% reflectivity provides the best correction.
- ✓ The model was used to correct the luminous flux of the samples, with the error bars for all samples containing the corrected flux.
- ✓ The uncertainty budget is affected by the present corrections, and it can be calculated (example of Sample #3).
- ✓ The model can be improved in future simulations by adding details of the hemisphere borders.
- ✓ In a subsequent study, experimental measurement of the SRDF can further advance the characterization of our equipment, as shown by Winter at al. [6].



References

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Thank you!

Questions?

